

isomerization reaction of compound 1 will be presented elsewhere.

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Surface tension of adsorbative in the Hill equation for polymolecular adsorption

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A simple and fairly exact expression for the b constant in the Hill equation of polymolecular adsorption is proposed:

$$\ln(p_s/p) = b\theta^{-3}, \quad (1)$$

where p is the equilibrium vapor pressure of an adsorbate; p_s is the saturation vapor pressure of a liquid at the temperature of the adsorbate; and θ is the adsorption in units of a dense monolayer. The expression for b is as follows:

$$b = 2.5\sigma_0 V_0 / (RTd), \quad (2)$$

where σ_0 and V_0 are the surface tension and molar volume of the adsorbate in the state of a normal liquid, respectively; d is the diameter of the molecules of the adsorbate; T is the temperature; and R is the universal gas constant.

In order to derive Eq. (2), let us compare two systems: I, the adsorption system consisting of an adsorption layer in the form of a liquid film on a planar surface of a solid adsorbent; and II, the "liquid" system that represents a bulk volume of a liquid with the planar liquid-vapor interface. In both systems, at the gas phase interface, a tangential pressure p_T exists that decreases when the distance (τ) from the boundary

surface of zero thickness increases. Let us assume that the known equation¹ holds for both systems:

$$p_T = p + C\tau^{-3}, \quad (3)$$

where C is the constant related to the parameters of interaction of the molecules of a liquid with each other and with the molecules of neighboring phases; p is an external pressure. Let us denote $C = C^I$ for the first system and $C = C^{II}$ for the second system. Previously,² the following expression was found for system I:

$$b = -3C^I V_0 / (RTd^3). \quad (4)$$

In order to estimate the C^{II} value for the second system, we assume that whole volume of a liquid, beginning from the boundary layer, is separated into layers one molecule thick that are parallel to the boundary layer. Let us denote the constant tangential pressure acting in the i layer and changing jumpwise from one layer to another as $p_{T,i}$. The tension of the i layer (σ_i), taking into account Eq. (3), is determined by the expression

$$\sigma_i = (p - p_{T,i})d = -C^{II}/(i^3 d^2),$$

where $\tau = id$. Apart from the critical temperature, it can be accepted with enough accuracy that the surface ten-

sion of a liquid at the vapor interface is equal to the sum of σ_i :

$$\sigma_0 = \sum_{i=1}^{\infty} (p - p_{T,i})d = -\left(C^{II}/d^2\right)\left(1 + \frac{1}{2^3} + \frac{1}{3^3} + \dots\right). \quad (5)$$

The sum in brackets that represents a convergent numerical series is approximately equal to 1.2. Then

$$C^{II} = -0.833\sigma_0 d^2. \quad (6)$$

Commonly, $C^I \neq C^{II}$, because the adsorption system, beginning already from the second layer, differs from a bulk liquid in the nature of its molecules. However, taking into account a fast decrease in the effect of lower molecular layers (see Eq. (5)), this difference can be neglected and it can be accepted that $C^I = C^{II}$. Inserting expression (6) into Eq. (4), we obtain the required Eq. (2), and hence, the equation of polymolecular adsorption takes the following form:

$$\ln(p_s/p) = 2.5\sigma_0 V_0 / (RTd\theta^3). \quad (7)$$

The validity of assumptions made is confirmed by the experimental data. Figure 1 presents a dependence of θ^{-3} on $\ln(p_s/p)$ for two systems *A* and *B*: *A* is the nitrogen adsorbed on nonporous hydrated silica at 77 K; and *B* is the benzene adsorbed on graphitized thermal carbon black (GTC) at 293 K. Points are the experimental data obtained earlier for the *A*³ and *B*⁴ systems. The θ values are calculated according to the equation

$$\theta = a/a_m,$$

where a is the adsorption; a_m is the monolayer capacity determined on the basis of the BET equation for system *A* and from the value of molecular area of benzene (0.39 nm²) and the known surface area of GTC for system *B*.

Solid lines in Fig. 1 are plotted on the basis of calculations according to Eq. (7) with the use of the σ_0 and V_0 values taken from the handbook⁵: for nitrogen at 77 K $\sigma_0 = 8.85 \cdot 10^{-3}$ N m⁻¹, $V_0 = 34.63$ cm³ mol⁻¹; for benzene at 293 K $\sigma_0 = 28.53 \cdot 10^{-3}$ N m⁻¹, $V_0 = 87.63$ cm³ mol⁻¹. The diameter of the adsorbate molecules is determined from the expression $d = (V_0/N)^{1/3}$, where N is Avogadro's number.

As can be seen in Fig. 1, the calculation results agree with the experimental data. It should be noted that the ordinate of experimental points is very sensitive to the a_m value, because it appears in the third power. A small variation, within a few percent, makes it possible to obtain practically complete agreement between the theo-

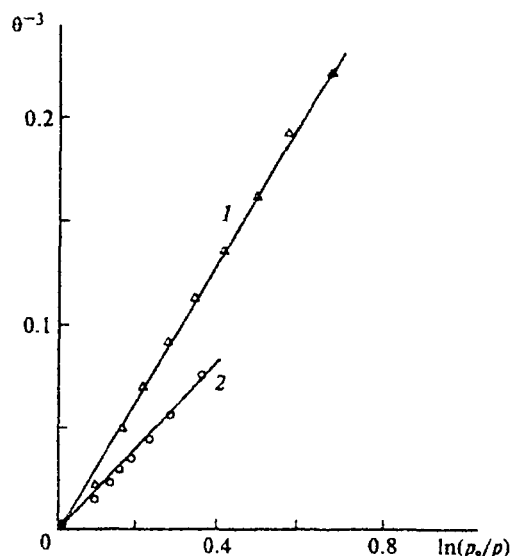


Fig. 1. Dependence of θ^{-3} on $\ln(p_s/p)$ for systems *A* (1) and *B* (2).

retical calculation and experimental data. This makes it difficult to verify Eq. (7), because the accuracy of the a_m determination by the BET method does not exceed 10%.

A correspondence between the calculated and experimental data allows one to consider Eq. (7) as a possible basis for an improved method for determining the specific surface area of nonporous adsorbents. In some cases, for example for the water—hydrocarbon adsorbent system, the calculations of a_m according to Eq. (7) are of special importance for the determination of the hydrophilic surface area.

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